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The Deployment of Supercritical Fluid Extraction for Moisture Measurements in Impure Plutonium Oxides

LA-UR-00-2911

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Applied Chemical Technology Group (C-ACT)

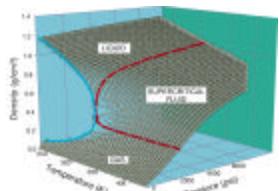
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^c Plutonium Metallurgy Group (NMT-16)

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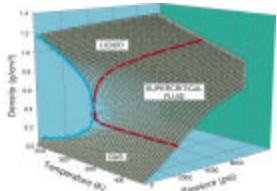


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Statement of the Problem with Long-term Storage of PuO₂

- Hydrogenous material mixed with pure/impure plutonium oxide powder may cause hydrogen production (through radiolysis) and pressurization of the welded canisters
- DOE-STD-3013-94/99 calls for material to be thermally stabilized by calcining at 950°C for at least two hours
- Thermal stabilization to be verified by Loss On Ignition at 1000 °C for at least one hour - weight loss not to exceed 0.5 mass %

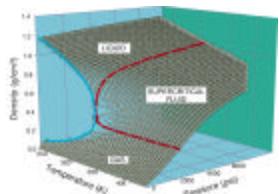
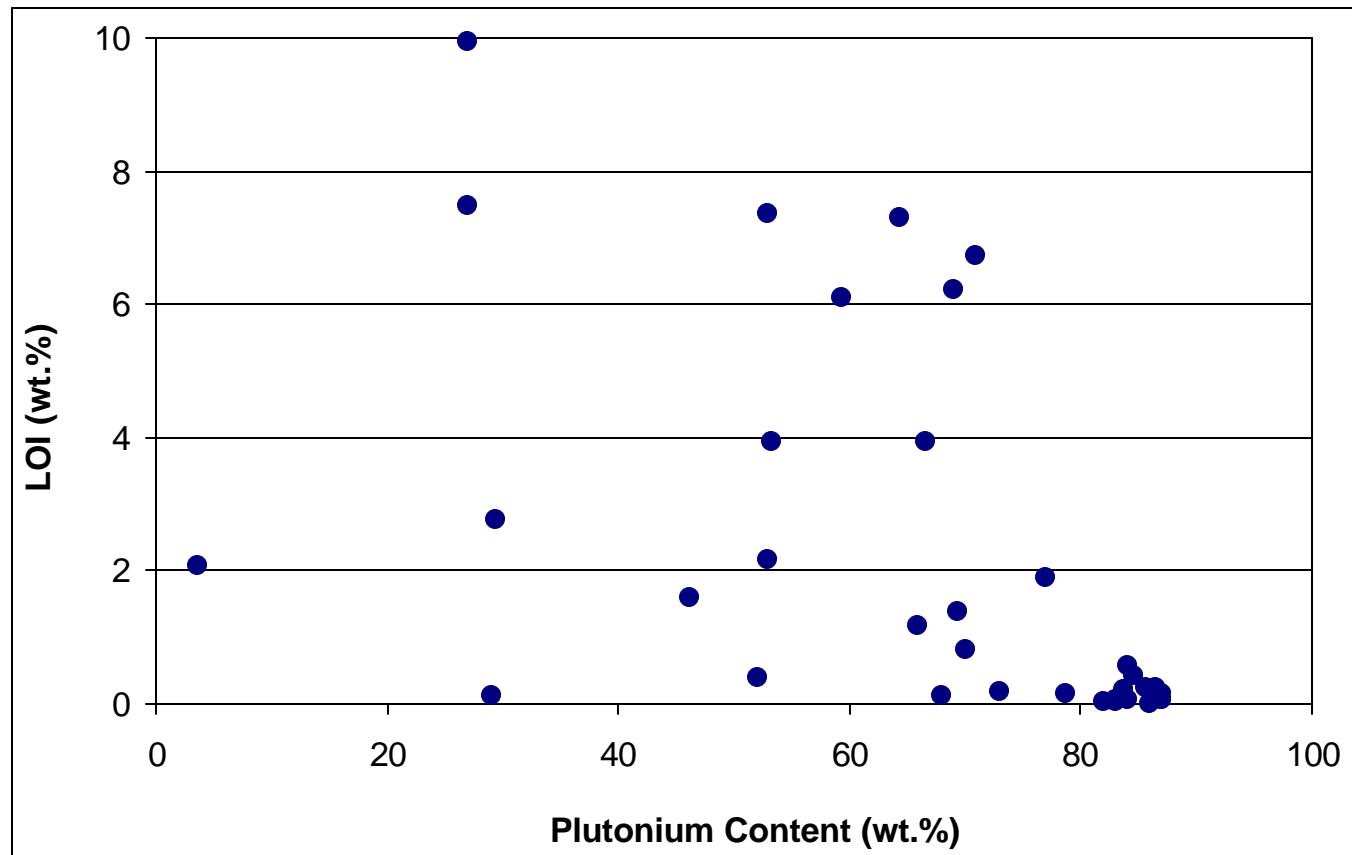


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Loss on Ignition

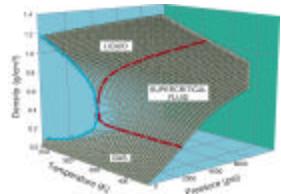
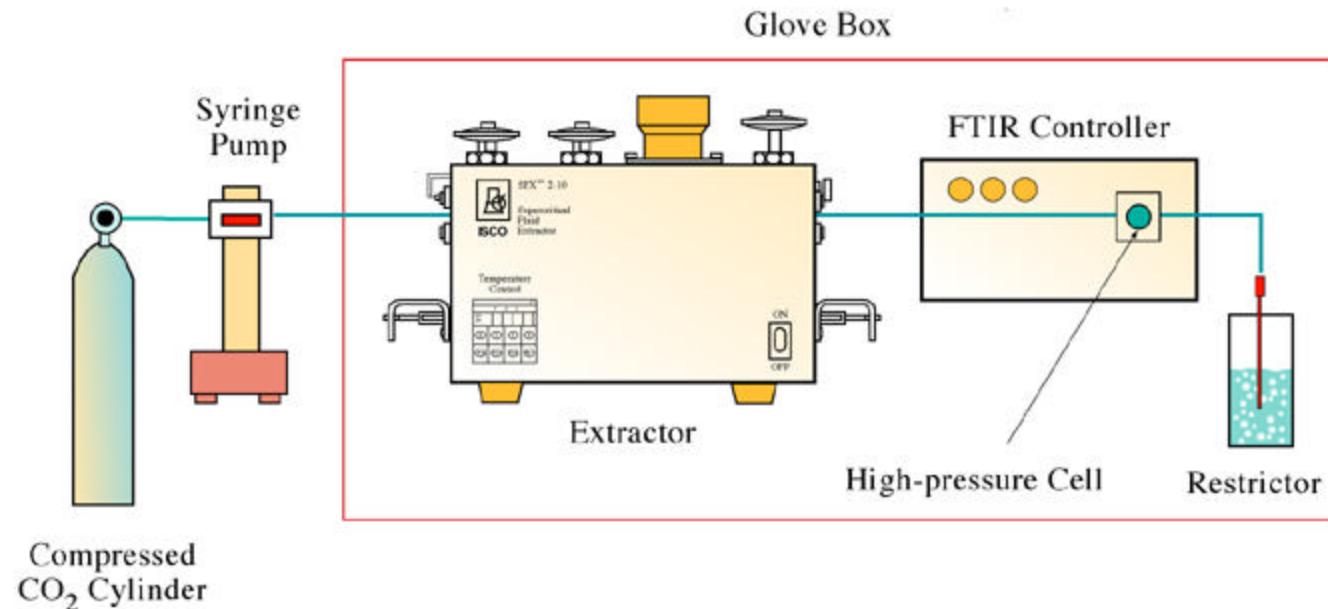
Unsuitability for Impure Materials



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SFE Schematic



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SFE - Requirements

- Initial capital cost

- $\approx 50 \text{ K}$

- Annual operating cost

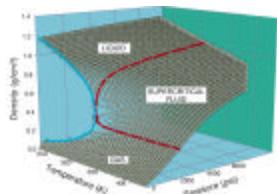
- $\approx 10 \text{ K}$

- Personnel requirements

- 1 technician (2-person rule observed)

- Facility requirements

- Glovebox



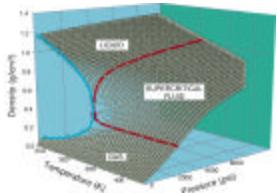
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SFE - Advantages

● Advantages

- Large sample size (± 20 g)
- Short analysis time (30 - 60 minutes)
- Minimal to no liquid waste generation
- Data collection is automatic
- DOE approved method



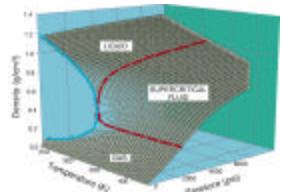
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SFE - Disadvantages

● Disadvantages

- Plugging with high salt samples
- FTIR window susceptible to acid attack
- Hydrates problematic

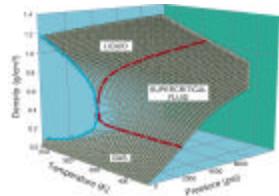
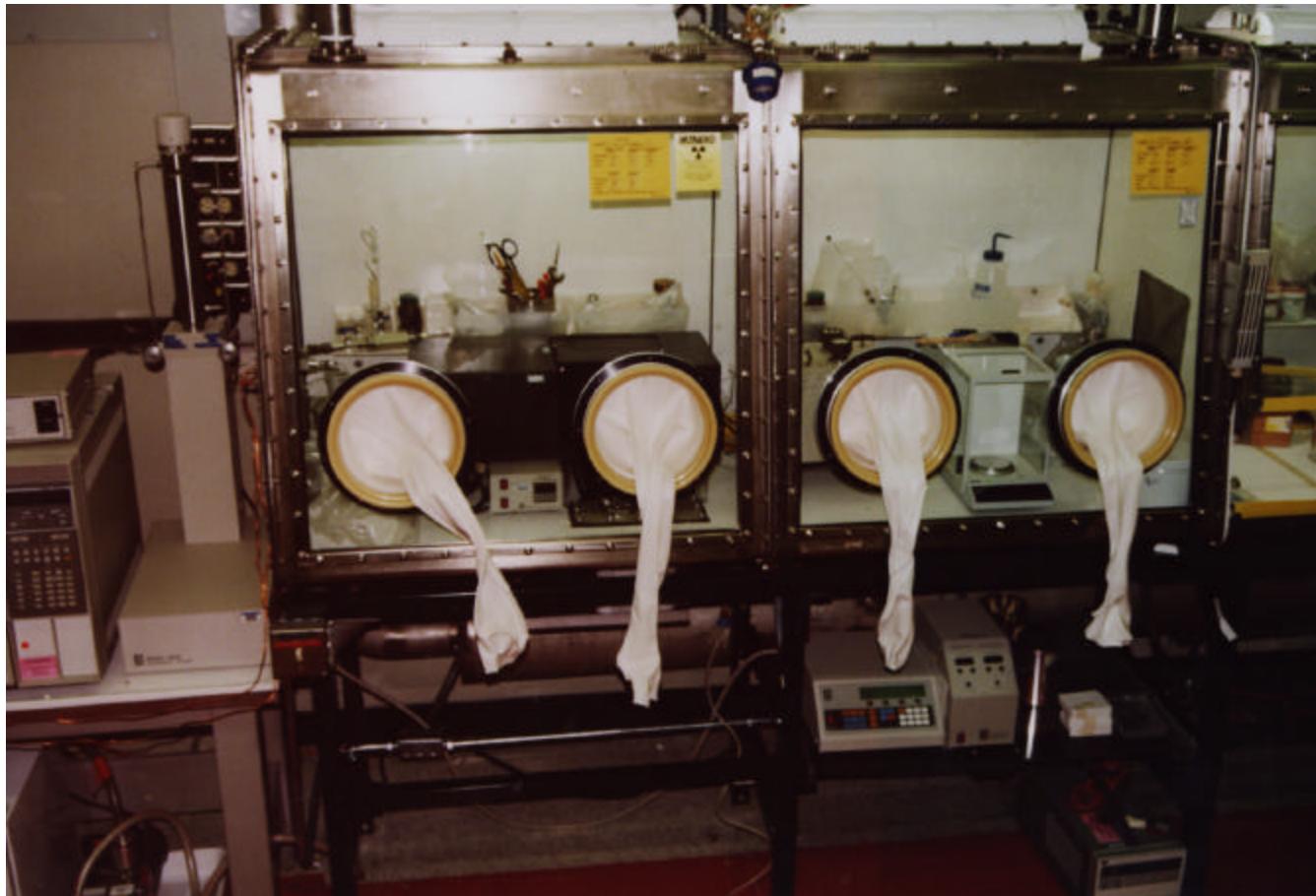


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LANL

SFE/FTIR Glovebox Assembly

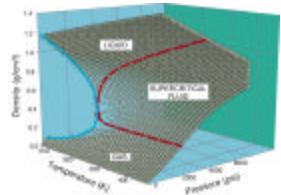
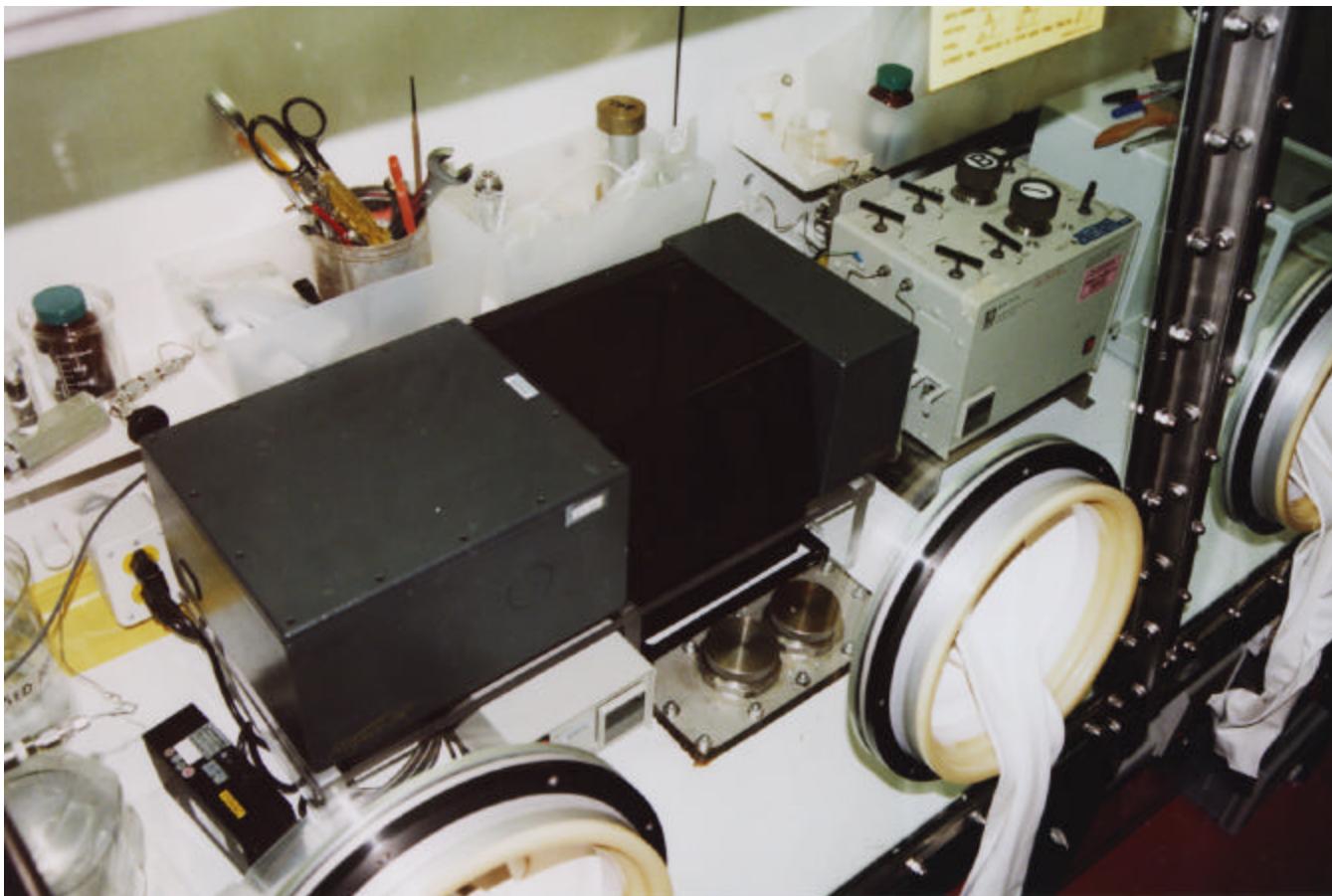


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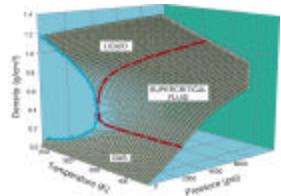
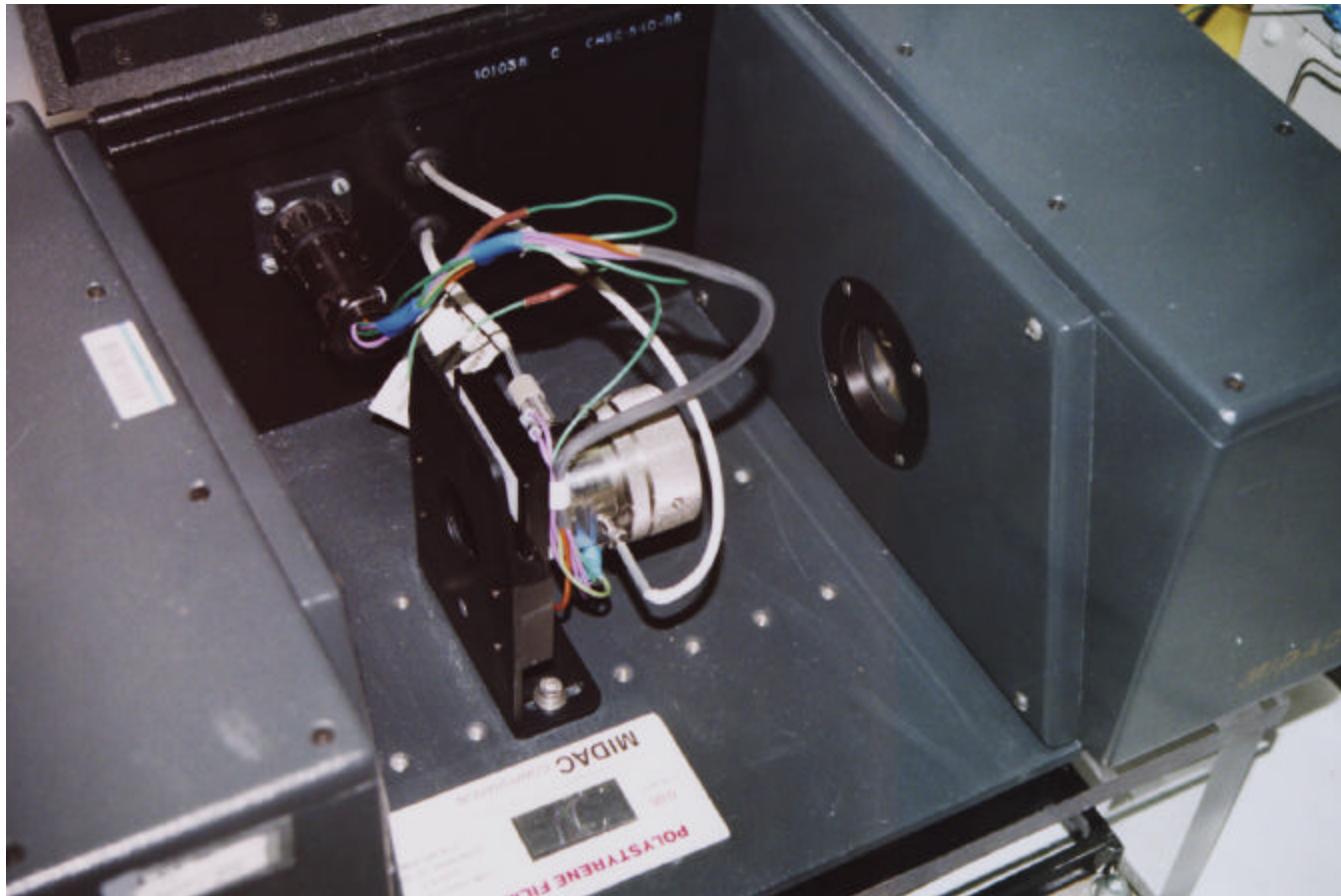
SFE/FTIR Glovebox Assembly



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High-Pressure FTIR Cell

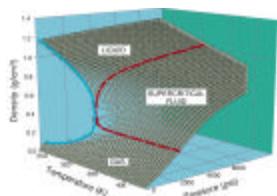


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Cumulative Work (SFE)

Extracted Matrix	Dates	Number of Extractions
Aluminum Oxide, Al_2O_3	9/96	3
Ammonium Molybdate, $(\text{NH}_4)_6\text{Mo}_7\text{O}_{24} \cdot 4\text{H}_2\text{O}$	4/97	2
Calcium Sulfate Dihydrate, $\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$	4/97 - 8/97	9
Cerium(IV) Oxide, CeO_2	12/96 - 8/97	28
Magnesium Sulfate Heptahydrate, $\text{MgSO}_4 \cdot 7\text{H}_2\text{O}$	9/96 & 5/97	4
Magnesium Phosphate Octahydrate, $\text{Mg}_3(\text{PO}_4)_2 \cdot 8\text{H}_2\text{O}$	5/99	3
Sodium Borate Decahydrate, $\text{Na}_2\text{B}_4\text{O}_7 \cdot 10\text{H}_2\text{O}$	5/99	3
Thorium Oxide, ThO_2	7/97	3
Water, H_2O	9/96 - 7/97	44
Zirconium Oxide, ZrO_2	9/96 - 3/97	15
Empty Vessels, Aluminum & PEEK	2/97 - 7/97	6
Plutonium Oxide, PuO_2	9/96 - present	123
Total Number of Extractions		243

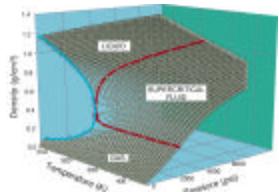


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LANL Observations

- 950°C calcine removes water
- Minimal water re-uptake in vault storage for most material tested
- For **VERY** pure oxides, LOI can be used for routine moisture analysis
- For impure oxides, LOI is unsuitable

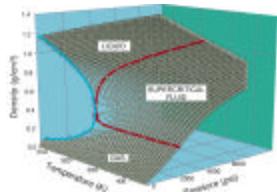


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Deployment Schedule - Supercritical CO₂ extraction

- Manufacturer has implemented design modifications to equipment for this application
- SFE to be installed at RFETS no later than 5/1/00
- SFE to be installed at Hanford (PFP) no later than 10/1/00

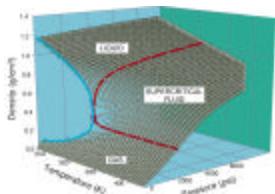


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Deployment Status - Supercritical CO₂ extraction - RFETS

- Bi-weekly conference calls initiated 12/3/99
- MOU signed on 12/14/99
- Design Criteria Document completed 1/17/00
- Equipment purchased by RFETS and procured by LANL on 2/18/00
- RFETS operators trained at LANL during the week of 2/21/00
- RFETS equipment shipped to RFETS on 3/3/00
- RFETS “cold” installation set for 4/3/00
- Installation in Glovebox 12/1/00

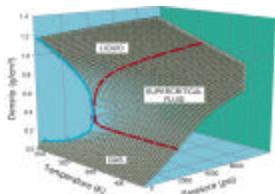


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Deployment Status - Supercritical CO₂ extraction –PFP

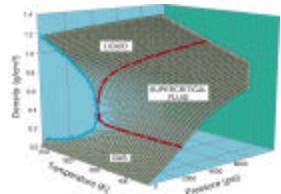
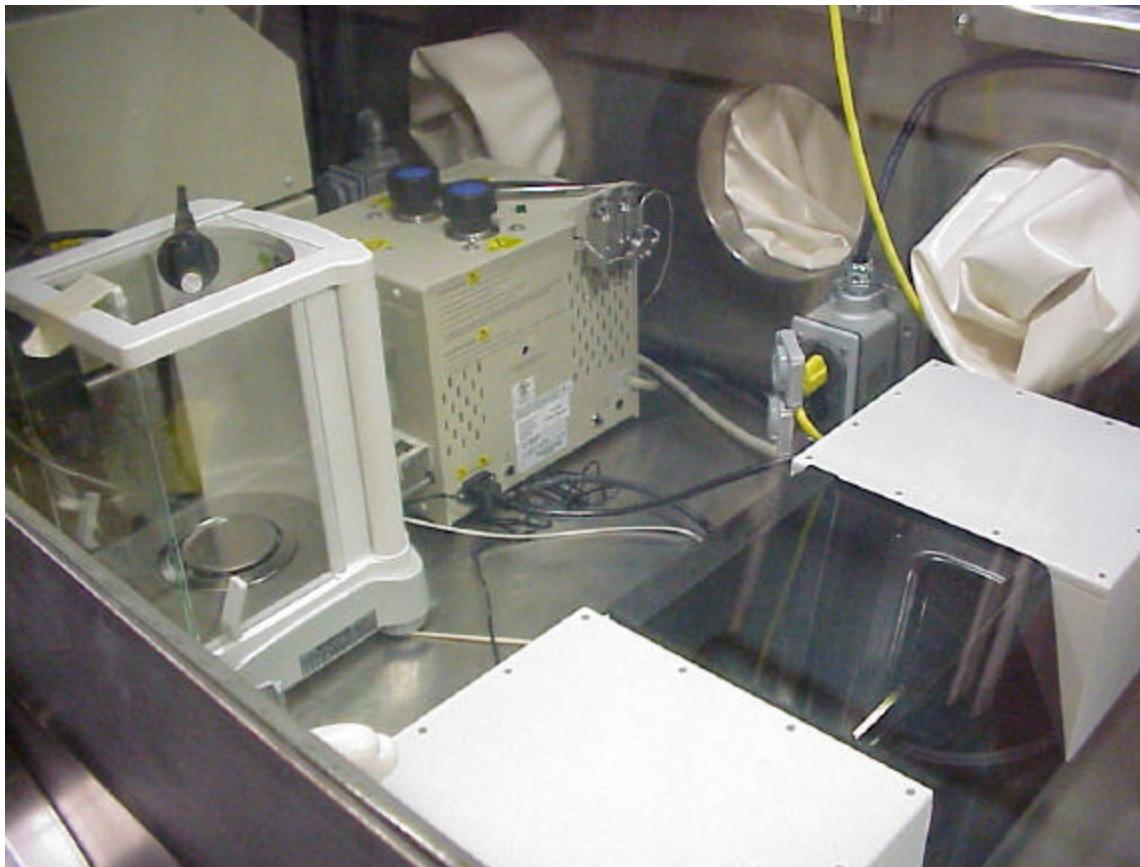
- Bi-weekly conference calls initiated 11/24/99
- MOU signed on 1/3/00
- Equipment purchased by PFP and shipped to LANL on 8/15/00
- PFP operators trained at LANL during the week of 8/28/00
- PFP equipment shipped 9/1/00
- PFP installation and pasted ORR 9/18/00
- Hot Samples Processed beginning 9/25/00



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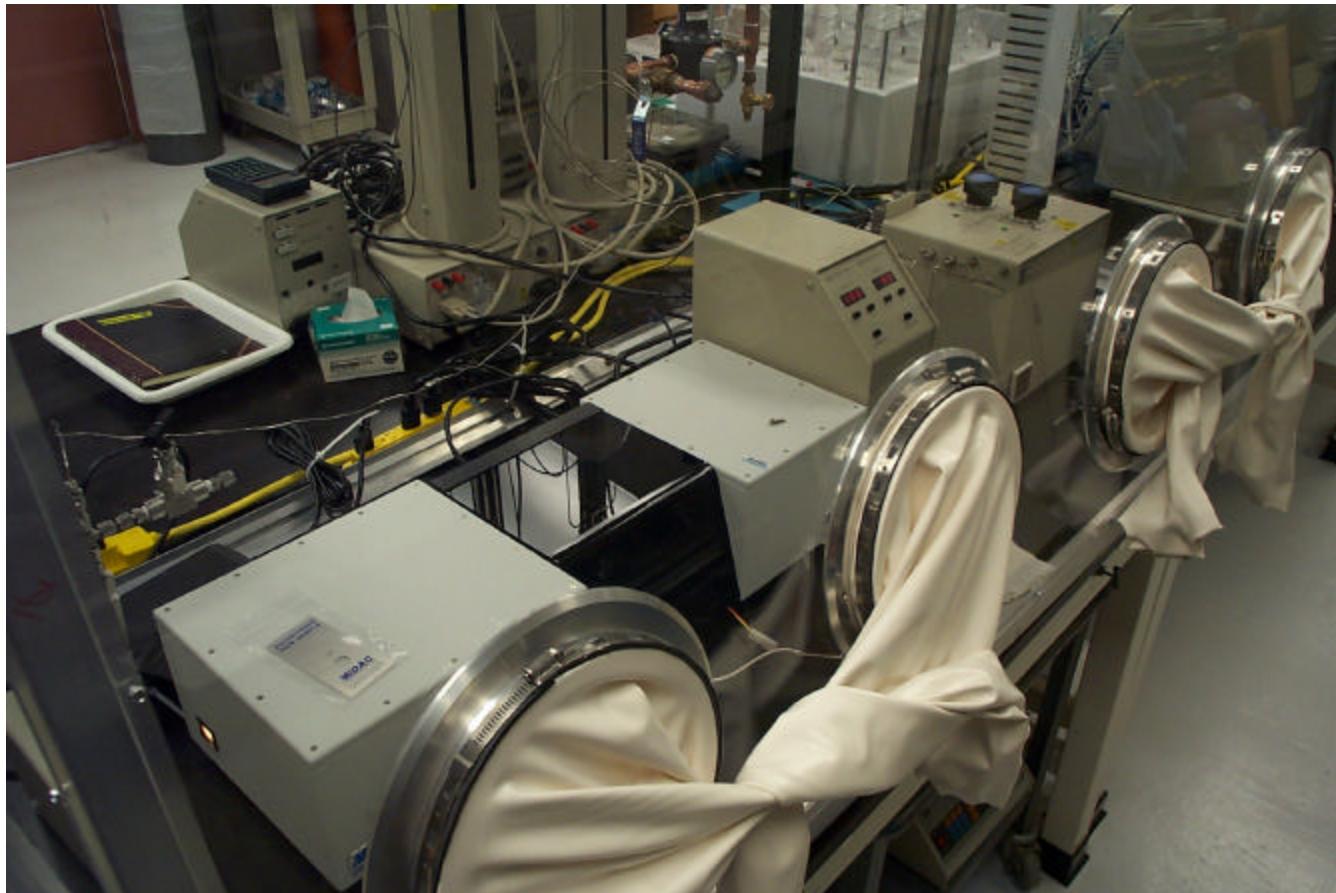
Installed SFE System at Hanford PFP



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RFETS/PFP Operator Training

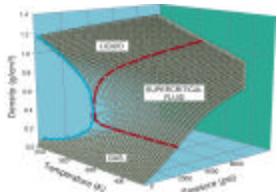


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Continuing Development of the SFE Technique

- Plugging with high salt (chloride) samples
 - Automated back-pressure regulator
- FTIR window susceptible to acid attack
 - Surveillance of samples (spot testing ?), alternate materials for windows
- Hydrates problematic
 - Thermal stabilization should address this
- Hydroxides



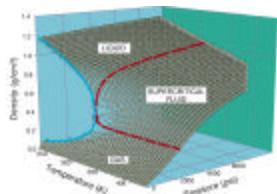
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- K Hakonson : *Applied Chemical Technology Group (C-ACT)*
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This work is performed as part of the 94-1 R&D Project (Rick Mason, Project Leader)



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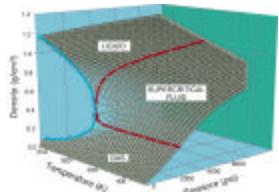
On-Line Resources

- MIS web-page :

w10.lanl.gov:80/orgs/nmt/nmt6/PuRD/index.htm

- Supercritical Fluids Facility web-page :

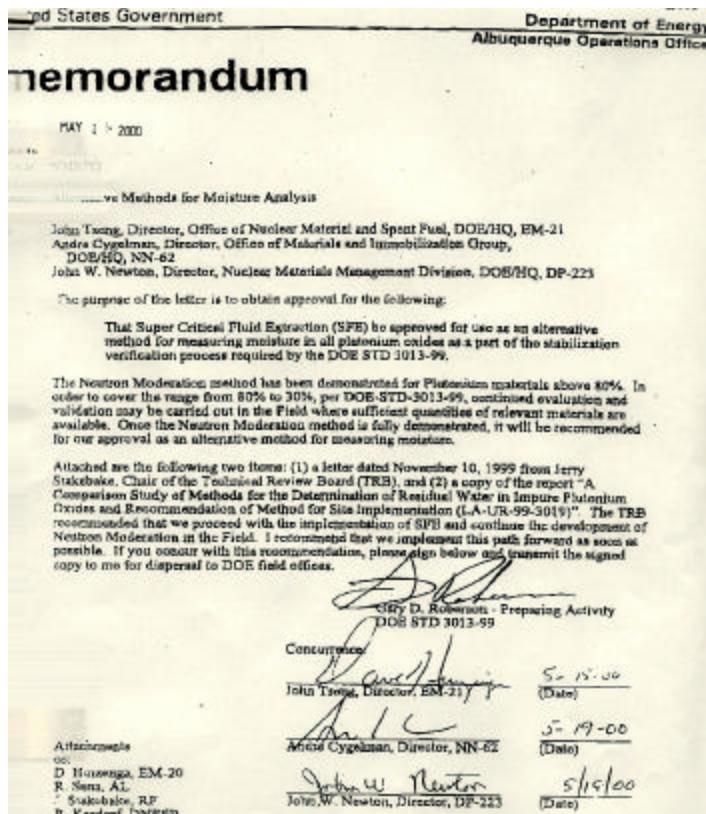
www.scrub.lanl.gov



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Alternative Method Approval



•Method approved for STD-3013-99 on May 19, 2000

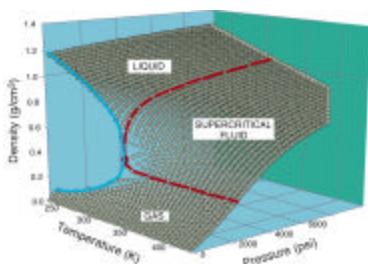
•“..alternative method for measuring moisture in all plutonium oxides..”

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Data Summary - CCLANL025

As-received, 0.06 wt.% H₂O	Measured moisture content, average wt. % loss	Standard deviation, s,¹ of the measurements and (number of runs)
LOI	7.79	1.08 (2)
IGA total H ₂ O (300°C) + total H ₂ (950°C) data	0.07	0.02 (3)
SFE	0.05	0.02 (2)
Neutron Moderation	0.31	0.03 (2)
<hr/>		
Spiked to 0.36 wt.% H₂O		
LOI	7.03	0.16 (2)
IGA, total H ₂ O (300°C)	0.40	0.01 (2)
IGA, total H ₂ (950°C)	0.41	0.06 (3)
SFE	0.54	0.16 (7)
Neutron Moderation	0.38	0.07 (2)
<hr/>		
Spiked to 0.74 wt.% H₂O		
LOI	6.83	0.04 (2)
IGA, total H ₂ O (300°C)	0.74	0.10 (3)
IGA, total H ₂ (950°C)	0.95	0.06 (3)
SFE	1.19	0.32 (7)
Neutron Moderation	0.63	0.01 (2)
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Re-calcined		
LOI	4.99	0.49 (2)
IGA, total H ₂ O (300°C)	< 0.03	— (3)
IGA, total H ₂ (950°C)	< 0.03	— (3)
SFE	< 0.03	— (2)
Neutron Moderation	0.37	0.04 (2)



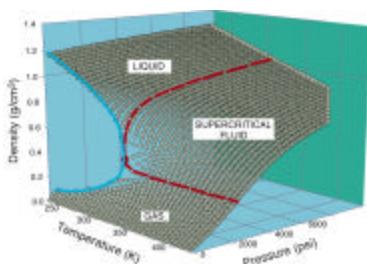
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Data Summary -

High Pu

($\text{MgSO}_4 \cdot 6\text{H}_2\text{O}$ spiked)

	Average moisture Content (wt. %)	Standard deviation, s^1 , of (n) moisture content measurements
As-received		
LOI	0.46	0.00 (2)
IGA @ 300°C	0.17	0.00 (2)
IGA @ 900°C	0.22	0.01 (2)
SFE	<0.03	— (2)
TGA @ 300°C	0.43	— (1)
TGA @ 1000°C	1.20	— (1)
Neutron Moderation	-0.01	— (1)
Spiked to 0.3 wt.% H₂O		
LOI	0.82	0.02 (2)
IGA @ 300°C	0.26	0.04 (3)
IGA @ 900°C	0.36	0.01 (3)
SFE	0.12	0.04 (6)
TGA @ 300°C	0.26	— (1)
TGA@ 1000°C	0.64	— (1)
Neutron Moderation	0.16	0.02 (3)
Spiked to 0.7 wt.% H₂O		
LOI	0.90	0.01 (2)
IGA @ 300°C	0.37	0.16 (3)
IGA @ 900°C	0.29	0.01 (3)
SFE	0.21	0.06 (7)
TGA @ 300°C	0.21	— (1)
TGA@ 1000°C	0.67	— (1)
Neutron Moderation	0.29	0.01 (3)
Re-calcined		
LOI	x.xx	x.xx (2)
IGA @ 300°C	—	— (x)
IGA @ 900°C	—	— (x)
SFE	<0.03	— (2)
TGA @ 300°C	<0.20	— (1)
TGA@ 1000°C	0.21	— (1)
Neutron Moderation	-0.08	0.03 (3)



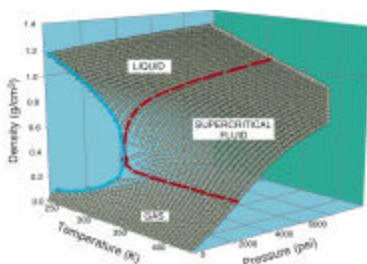
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Data Summary -

High Pu

($\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$ spiked)

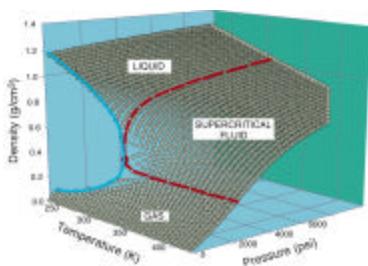
	Average moisture Content (wt. %)	Standard deviation, s , of (n) moisture content measurements
As-received		
LOI	0.23	< 0.01 (2)
IGA @ 300°C	0.02	0.00 (2)
IGA @ 900°C	0.06	0.01 (2)
SFE	< 0.03	— (1)
Neutron Moderation	-0.03	0.00 (2)
Spiked to 0.3 wt.% H₂O		
LOI	1.07	0.02 (2)
IGA @ 300°C	0.36	0.02 (2)
IGA @ 900°C	0.37	0.04 (2)
SFE	0.31	0.04 (7)
Neutron Moderation	0.20	0.05 (2)
Spiked to 0.7 wt.% H₂O		
LOI	1.25	— (1)
IGA @ 300°C	0.63	0.08 (2)
IGA @ 900°C	0.70	0.01 (2)
SFE	0.67	0.03 (6)
Neutron Moderation	0.73	0.10 (2)
Re-calcined		
LOI	x.xx	x.xx (2)
IGA @ 300°C	0.02	0.00 (2)
IGA @ 900°C	0.03	0.00 (2)
SFE	< 0.03	— (2)
Neutron Moderation	-0.10	0.05 (2)



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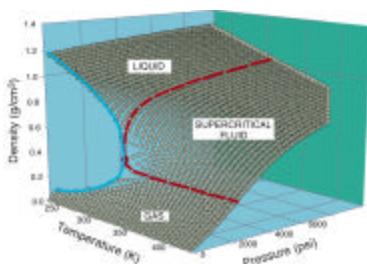
Data Summary - High U

	Average moisture Content (wt. %)	Standard deviation, s^1 , of (n) moisture content measurements		
As-received, pre-calcined				
LOI	-2.09	0.16	(2)	
IGA @ 300°C	0.17	0.00	(2)	
IGA @ 900°C	0.22	0.01	(2)	
SFE	0.05	0.01	(2)	
Neutron Moderation	-0.18	0.03	(3)	
As-received, calcined				
LOI	0.02	0.08	(2)	
IGA @ 300°C	< 0.03	—	(2)	
IGA @ 900°C	< 0.03	—	(2)	
SFE	< 0.03	—	(2)	
Neutron Moderation	-0.13	0.01	(2)	
Spiked to 0.3 wt.% H₂O				
LOI	1.07	0.02	(2)	
IGA @ 300°C	0.34	0.04	(2)	
IGA @ 900°C	0.39	0.01	(2)	
SFE	0.34	0.02	(7)	
Neutron Moderation	0.08	0.01	(2)	
Spiked to 0.7 wt.% H₂O				
LOI	9.45	9.78	(2)	
IGA @ 300°C	0.65	0.08	(2)	
IGA @ 900°C	0.61	0.05	(2)	
SFE	0.73	0.02	(7)	
Neutron Moderation	0.56	0.02	(3)	
Re-calcined				
LOI	1.05	0.02	(2)	
IGA @ 300°C	0.12	0.01	(2)	
IGA @ 900°C	0.13	0.00	(2)	
SFE	< 0.03	—	(2)	
Neutron Moderation	-0.05	0.02	(3)	



Data Summary - High Mg

	Average moisture Content (wt. %)	Standard deviation, s_1 of (n) moisture content measurements	
As-received, pre-calcined			
LOI	2.84	0.75	(2)
IGA @ 300°C	0.46	0.03	(2)
IGA @ 900°C	0.42	0.18	(3)
SFE	0.08	0.01	(2)
TGA	1.72	—	(1)
Neutron Moderation	0.25	0.08	(2)
As-received, calcined			
LOI	4.15	0.24	(2)
IGA @ 300°C	0.26	0.01	(2)
IGA @ 900°C	0.29	0.01	(2)
SFE	< 0.03	—	(2)
TGA	2.15	—	(1)
Neutron Moderation	0.02	0.02	(2)
Spiked to 0.06 wt.% H₂O			
LOI	3.68	0.65	(2)
IGA @ 300°C	0.37	0.05	(2)
IGA @ 900°C	0.29	0.19	(3)
SFE	0.06	0.03	(7)
TGA	2.17	—	(1)
Neutron Moderation	- 0.01	0.12	(2)
Spiked to 0.15 wt.% H₂O			
LOI	3.90	0.12	(2)
IGA @ 300°C	0.45	0.05	(2)
IGA @ 900°C	0.42	0.01	(2)
SFE	0.16	0.01	(7)
TGA	1.77	—	(1)
Neutron Moderation	0.07	0.06	(2)



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Data Summary - High Mg

Spiked to 0.3 wt.% H₂O

LOI	3.74	0.13	(2)
IGA @ 300°C	0.70	0.01	(2)
IGA @ 900°C	0.68	0.01	(2)
SFE	0.32	0.02	(7)
TGA	1.80	—	(1)
Neutron Moderation	0.08	0.01	(2)

Spiked to 0.5 wt.% H₂O

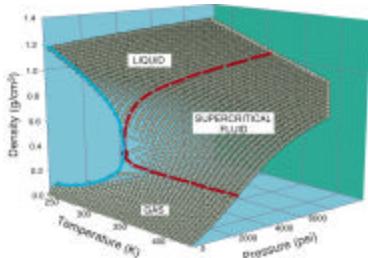
LOI	3.36	0.16	(2)
IGA @ 300°C	0.55	0.02	(2)
IGA @ 900°C	0.87	0.01	(2)
SFE	0.49	0.04	(7)
TGA	1.94	—	(1)
Neutron Moderation	0.44	0.07	(2)

Spiked to 0.7 wt.% H₂O

LOI	4.01	0.16	(2)
IGA @ 300°C	1.09	0.00	(2)
IGA @ 900°C	1.29	0.01	(2)
SFE	0.72	0.06	(4)
TGA	2.28	—	(1)
Neutron Moderation	0.74	0.01	(2)

Re-calcined

LOI	3.31	0.04	(2)
IGA @ 300°C	0.19	0.02	(2)
IGA @ 900°C	0.47	0.04	(3)
SFE	0.03	—	(1)
TGA	1.64	—	(1)
Neutron Moderation	-0.08	0.07	(2)



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